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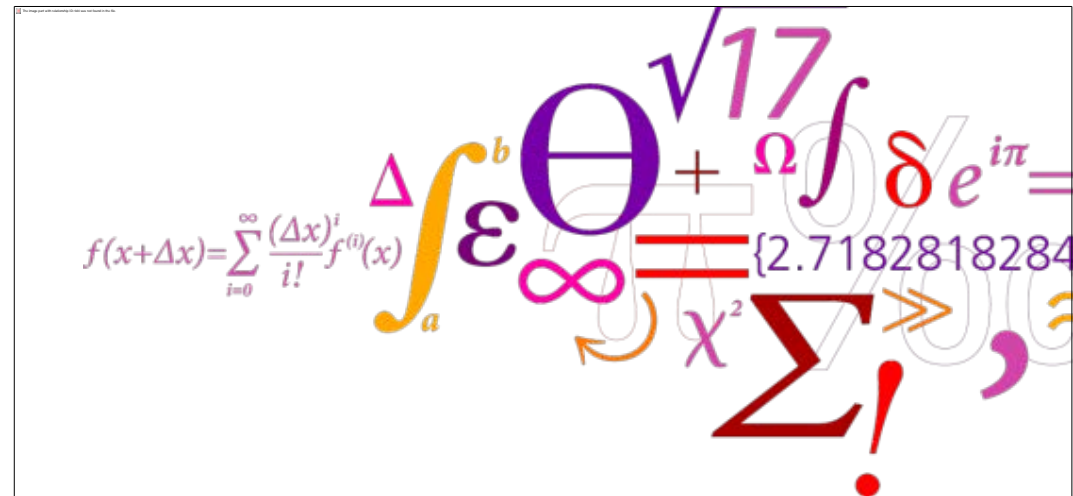
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A framework for medium-fidelity wake dynamics in moderately complex terrain

G.C. Larsen, P. van der Laan and S. Ott



Outline

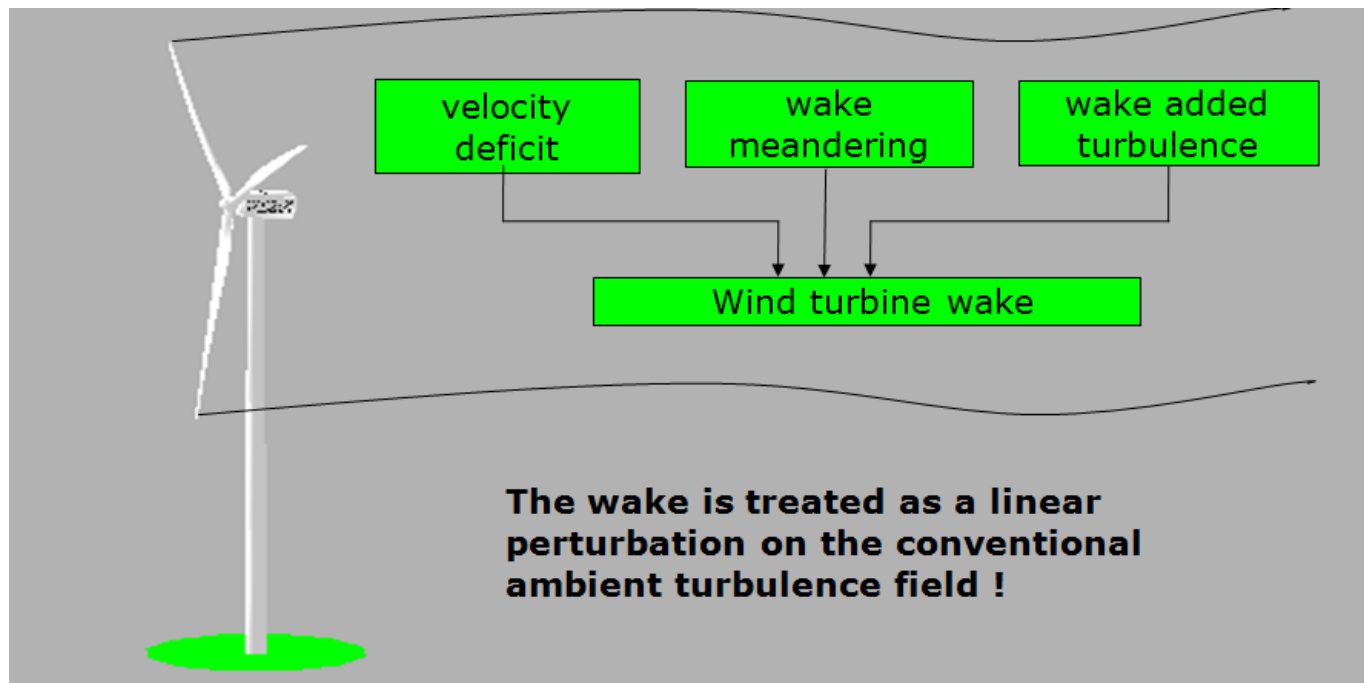
- Motivation
- DWM “classic” for flat terrain
- Generalization of DWM to “moderately” complex terrain
 - Definition of “moderately” complex terrain
 - Wake down-stream advection path
 - Wake deficit in MFor
 - Wake down-stream advection velocity
 - Stochastic wake meandering
 - Fast computation of stream lines and speed up in “moderately” complex terrain
- Conclusions
- Future work

Motivation

- *Non-stationary* flow fields are required for WT **load estimation**, facilitates WT **power production** estimation ... and thus WF **topology optimization**
- High-fidelity CFD-LES modeling is CPU-costly ... and a coupled aeroelastic/CFD-LES approach is **not** feasible for a large number of WF simulations!
- Need for medium-fidelity flow field models that
 - Preserves the **essential physics** of non-stationary wake flows
 - Is (relatively) **in-expensive**
 - Allow for a straight forward **coupling** with aeroelastic models

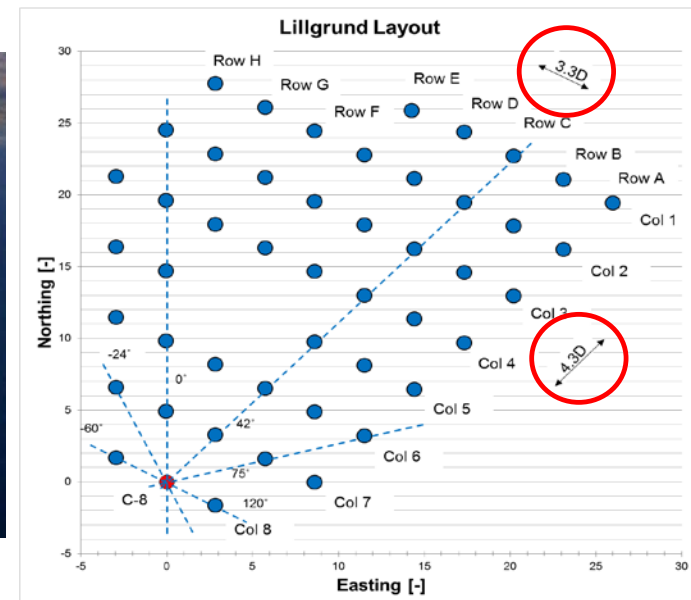
DWM “classic” (1)

- Included in the IEC-code as recommended practice
- Flat and homogeneous terrain (streamlines, turbulence)
- “Poor man’s LES” ... based on a **passive tracer** analogy
[Larsen GC et al.; Wake meandering – a pragmatic approach; WE]



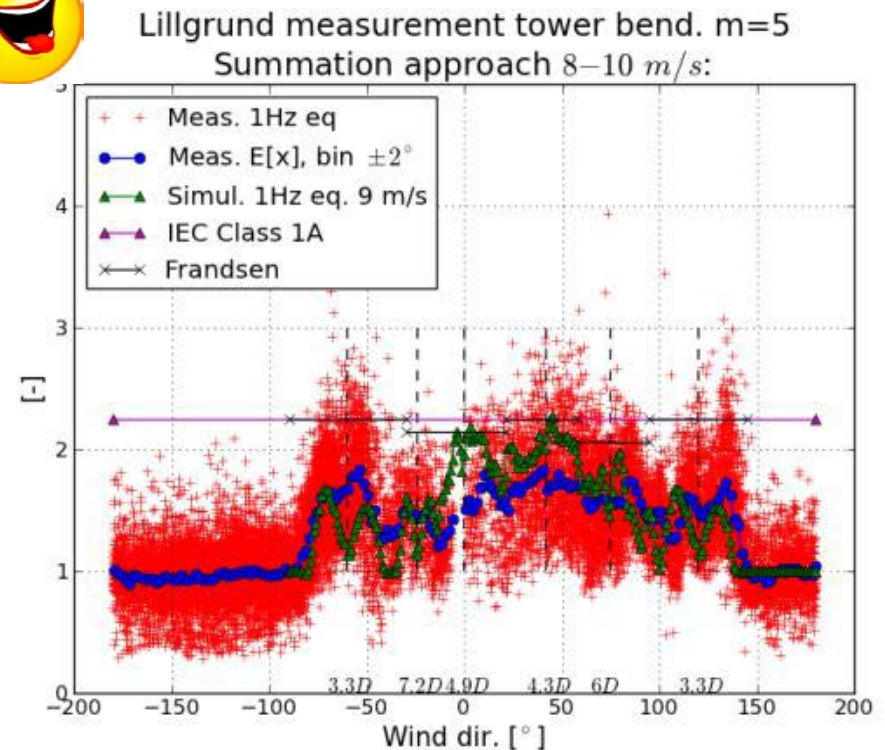
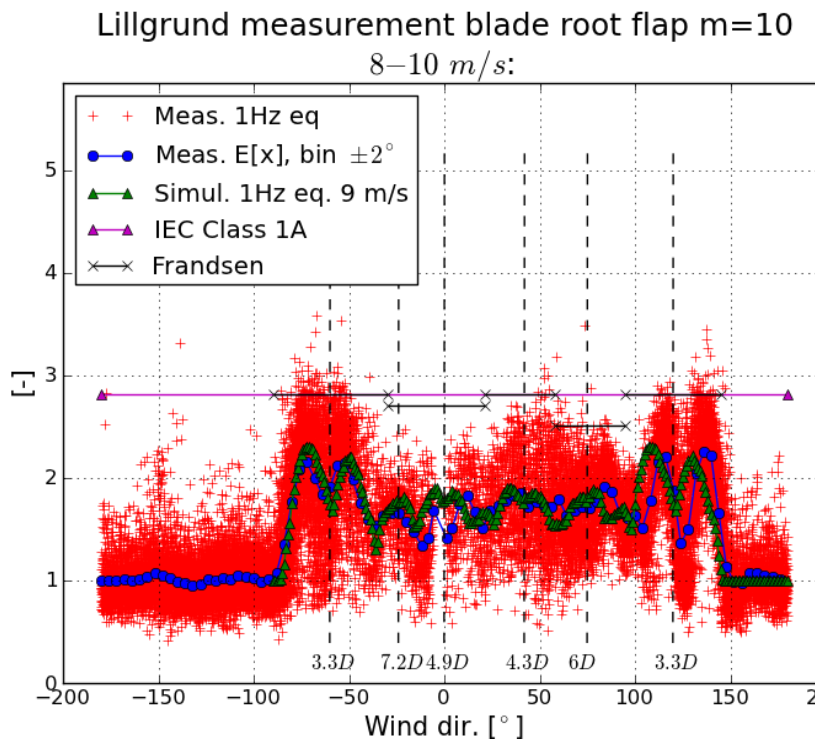
DWM “classic” (2) – does it work?

- 48 SWT 2.3 MW PRVS turbines
- Lowest spacing is 3.3D
- Turbine C-8 is fully instrumented with strain gauges ... blade and tower bending moments are available



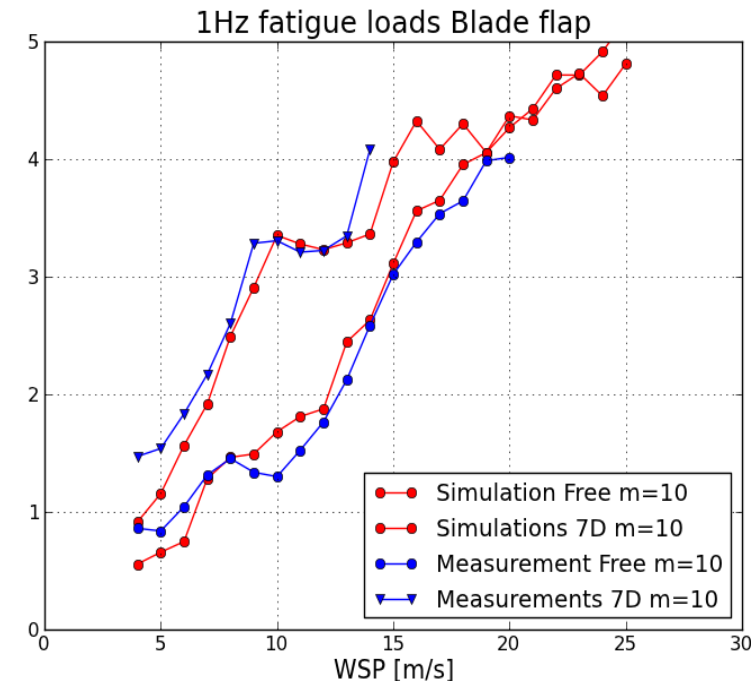
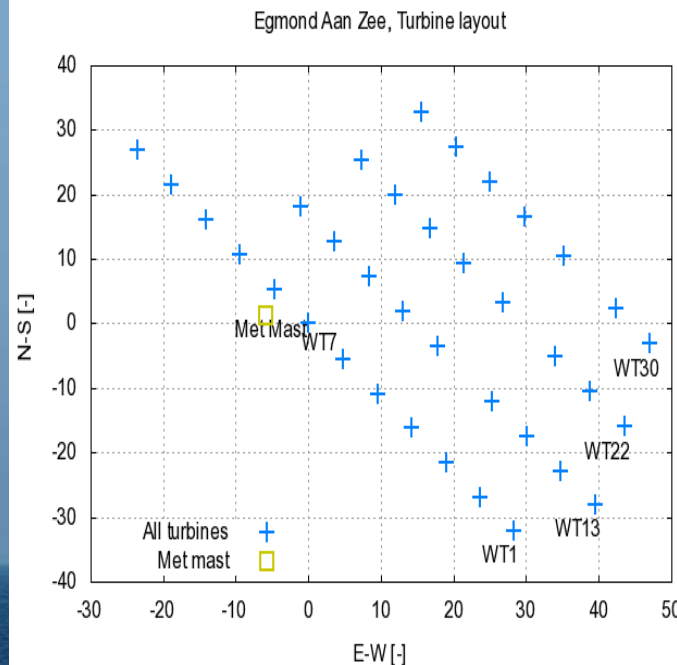
DWM “classic” (3) – does it work?

- Flap and tower bottom fatigue equivalent moments
 - 9m/s [Larsen TJ et al.; EWECC 2015]



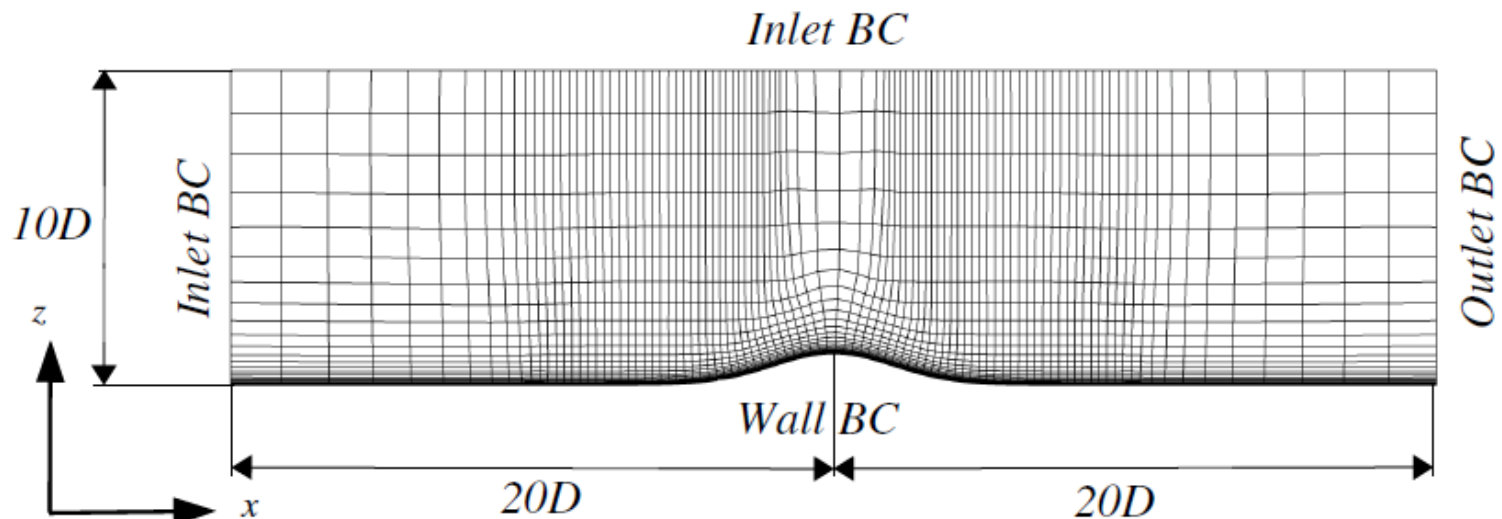
DWM “classic” (4) – does it work?

- Egmond Aan Zee - a farm of 36 Vestas 3MW V90 turbines
- Load and production compared for WT7 in free sector and full wake sector ($\sim 315^\circ$)



Generalization of DWM – “complex” terrain (1)

- “Moderately” complex terrain defined as orographics with no re-circulation ... in terms of **critical gradient**
- 2D Gaussian hill + EllipSys3D RANS simulations
- Separation occurs if the skin friction coefficient becomes negative



- 384 and 128 cell are used in the horizontal and vertical dimension ... grid independent results

Generalization of DWM – “complex” terrain (2)

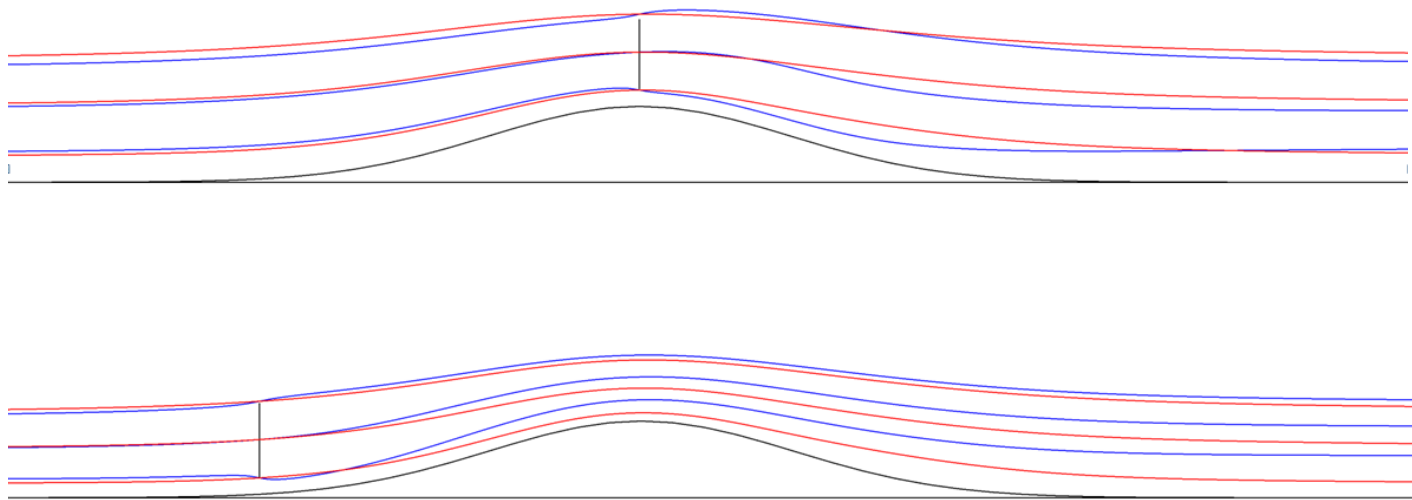
- Separation on the Gaussian hill is investigated for:
 - Different slope angles ... (16° - 21°)
 - 8.0 m/s ... and neutral logarithmic profile
 - Three roughness lengths ... (1 m, 0.1 m and 0.03)
 - Two turbulence models ... ($k-\epsilon$ and $k-\epsilon-f_p$)

Turbulence model	$z_0 = 0.03$ m	$z_0 = 0.1$ m	$z_0 = 1.0$ m
$k-\epsilon$	21°	19°	17°
$k-\epsilon-f_p$	20°	18°	17°

- Critical gradient in [this context](#) defined as 17°
 [...other studies have come to a similar result – e.g. WAsP CFD]

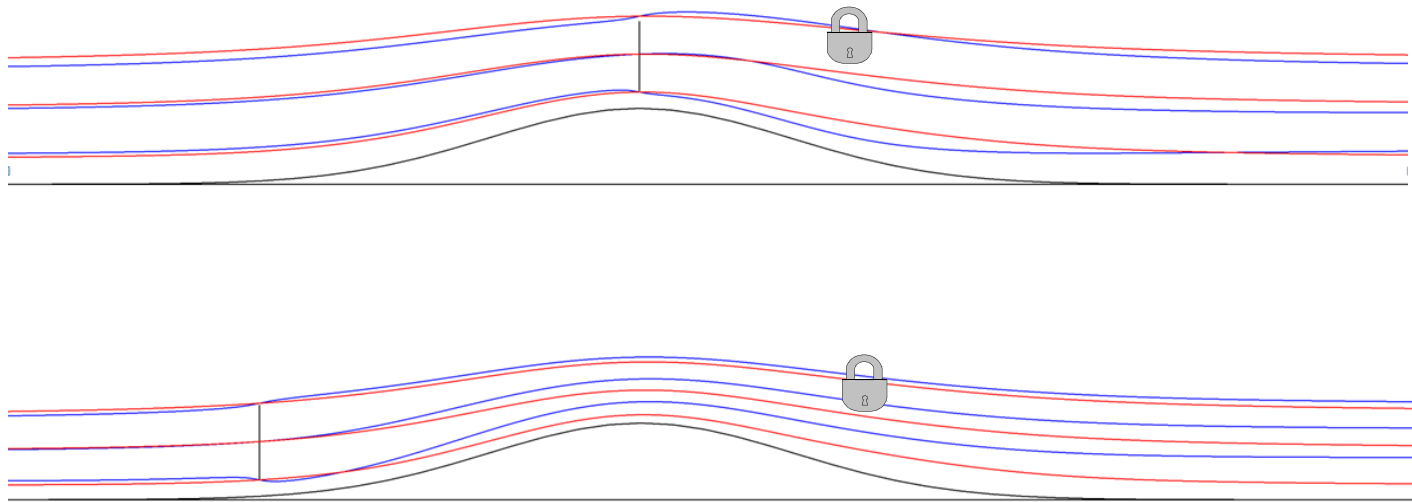
Wake downstream advection (1)

- Stream lines (17°) ... blue wake affected; red no wake



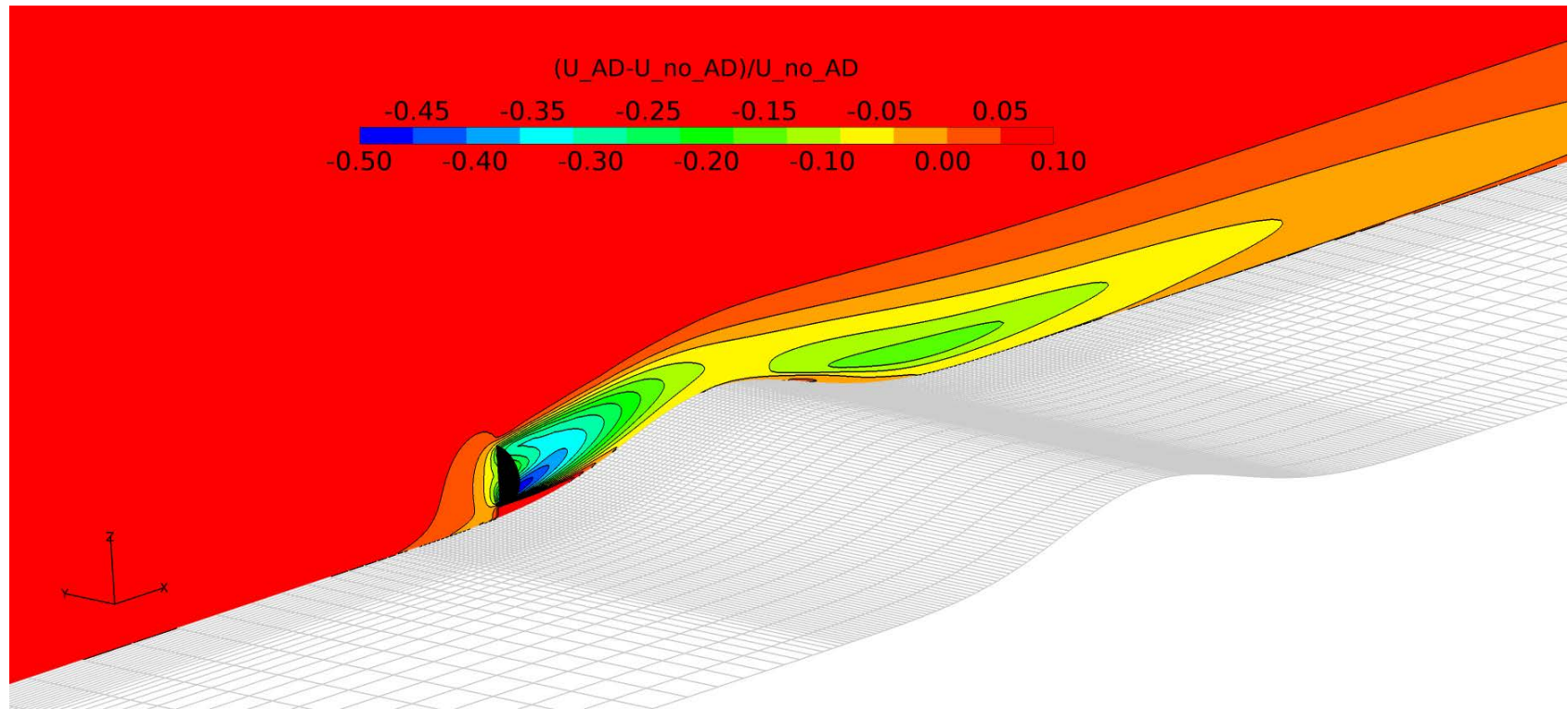
Wake downstream advection (2)

- Stream lines (17°) ... **blue** wake affected; **red** no wake



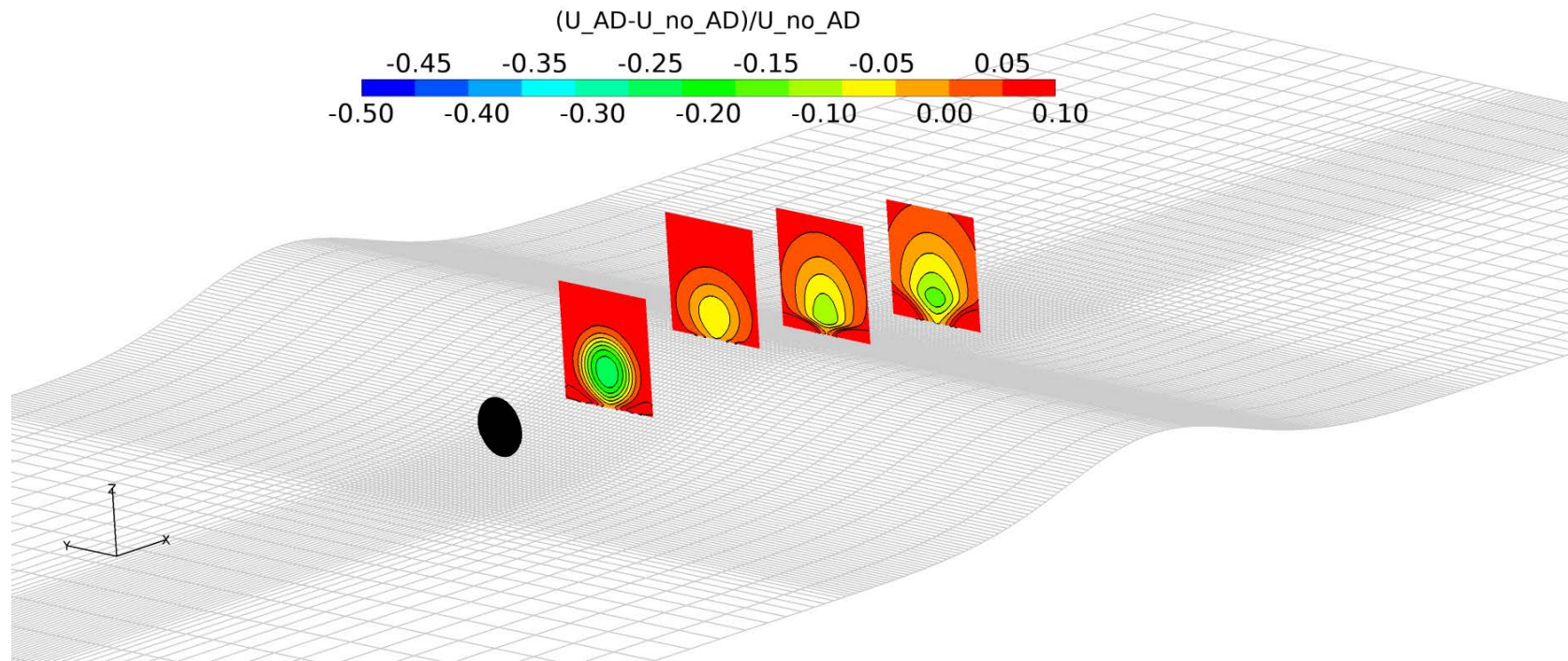
- 1'st conjecture:** In the vicinity of the hill, the **highest altitude** stream line match the best!

Wake deficit in MFor (1)



- Wake “follows” the hill in curve-linear coordinates ... as also indicated by the stream-line analysis
- NOT true for separated flows!

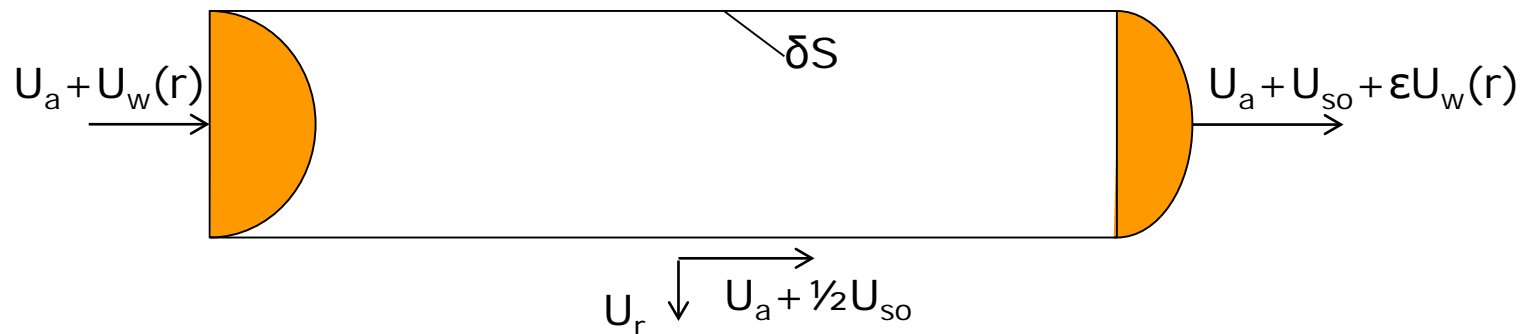
Wake deficit in MFor (2)



- **2nd conjecture:** Wake expansion is not significantly affected by hill speedup " $= >$ "
- **3rd conjecture:** Wake deficit scales under a similarity presumption

Wake deficit in MFor (3)

- Wake deficit scales under a similarity presumption:
 $U_{w,\text{speedup}}(r) = \varepsilon U_{w,\text{ambient}}(r)$
- The similarity assumption is restricted to the **dominating** along wind wake component



- **Continuity equation** yields $\int_{\delta S} U_r dS$ as function of the (idealized) along wind velocity components

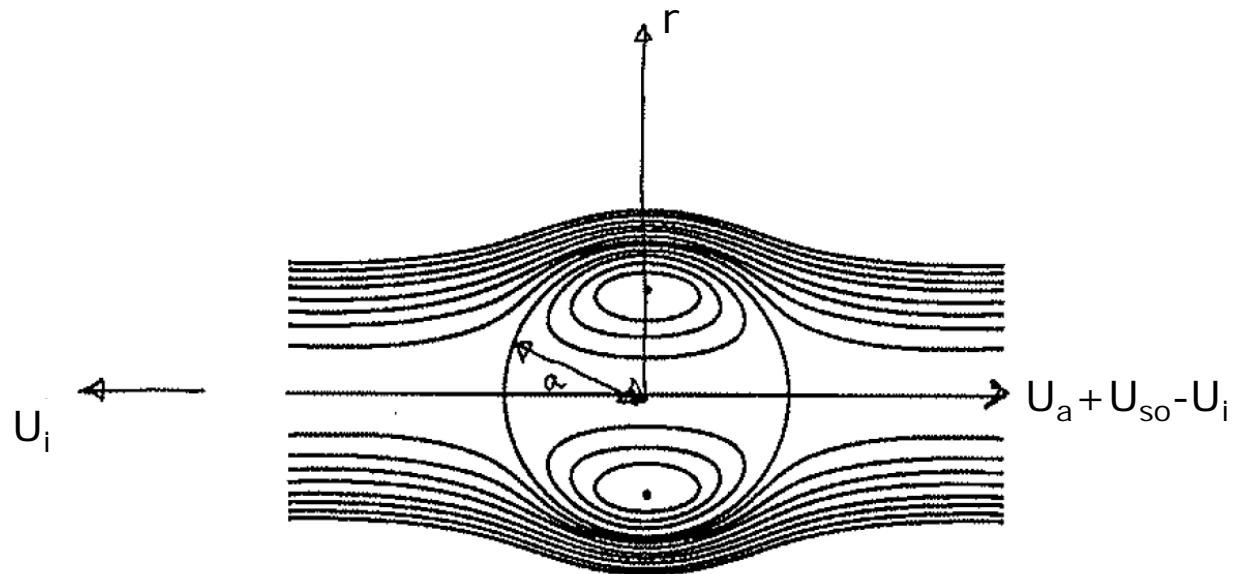
Wake deficit in MFor (4)

- **Momentum flux** in the mean flow direction pr. unit time across the surface of the control volume yields:

$\varepsilon = f(U_a, U_{so}, U_w)$... a simple algebraic expression

Wake downstream advection velocity

- 4'th conjecture: Advection based on a Hill's vortex approach and a rotor averaged wind speed ($U_a + U_{so}$) ... in the relevant flow domain [Lamp, 1932]



- $U_{adv} = U_a + U_{so} - U_i = U_a + U_{so} - 0.4\epsilon U_w(0) \dots$ along streamline

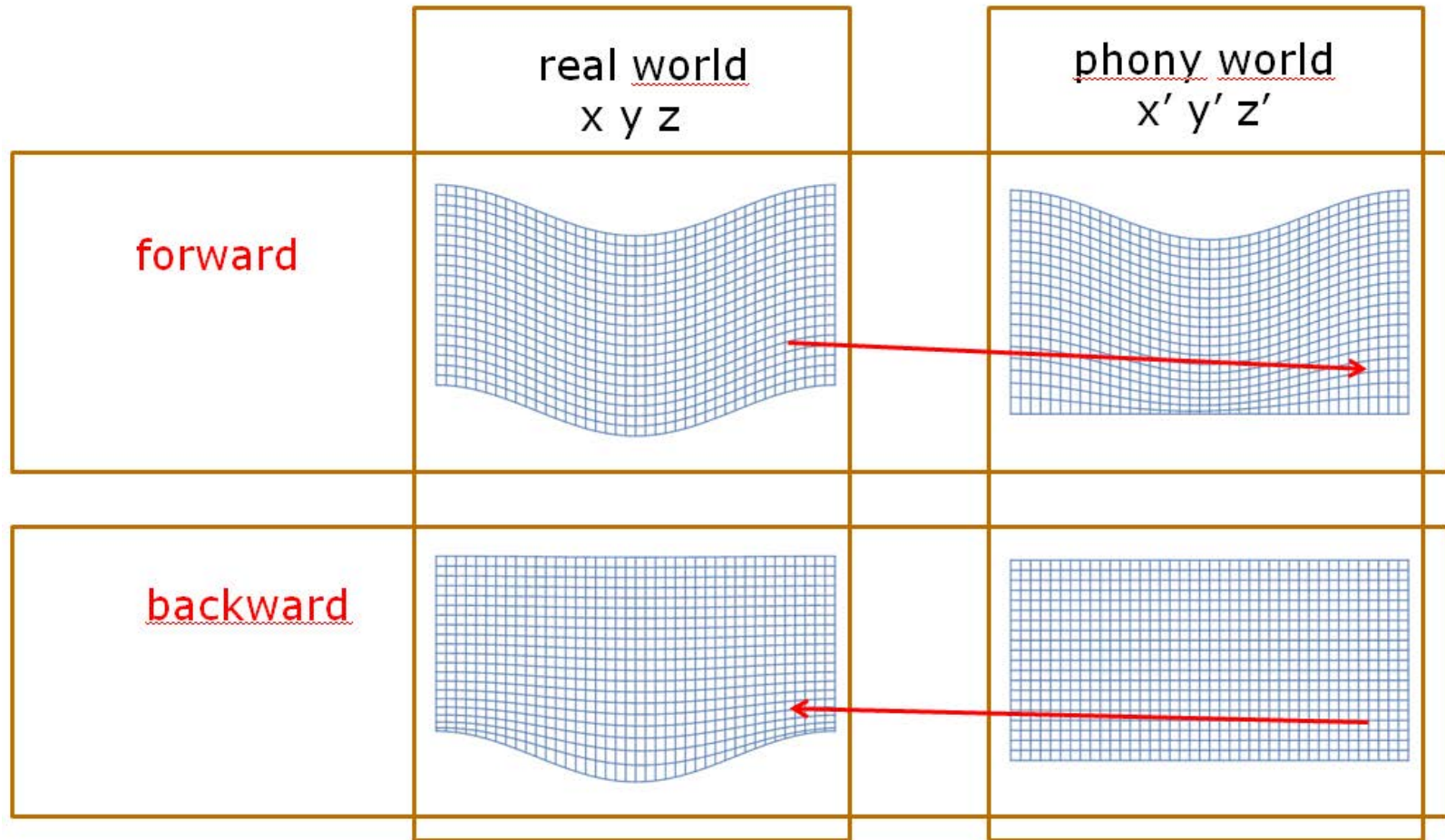
Stochastic wake meandering

- Wake meandering (laterally, vertically) **around streamline** driven by large scale ABL turbulence ... cut off frequency $U/2D$
- **5'th conjecture:** Conventional anisotropic ABL turbulence for flat terrain can be used ... expressed in a Cartesian frame of reference
- Mann spectral tensor used for neutral conditions
- A generalized spectral tensor used for non-neutral conditions ... consistently including buoyancy effects

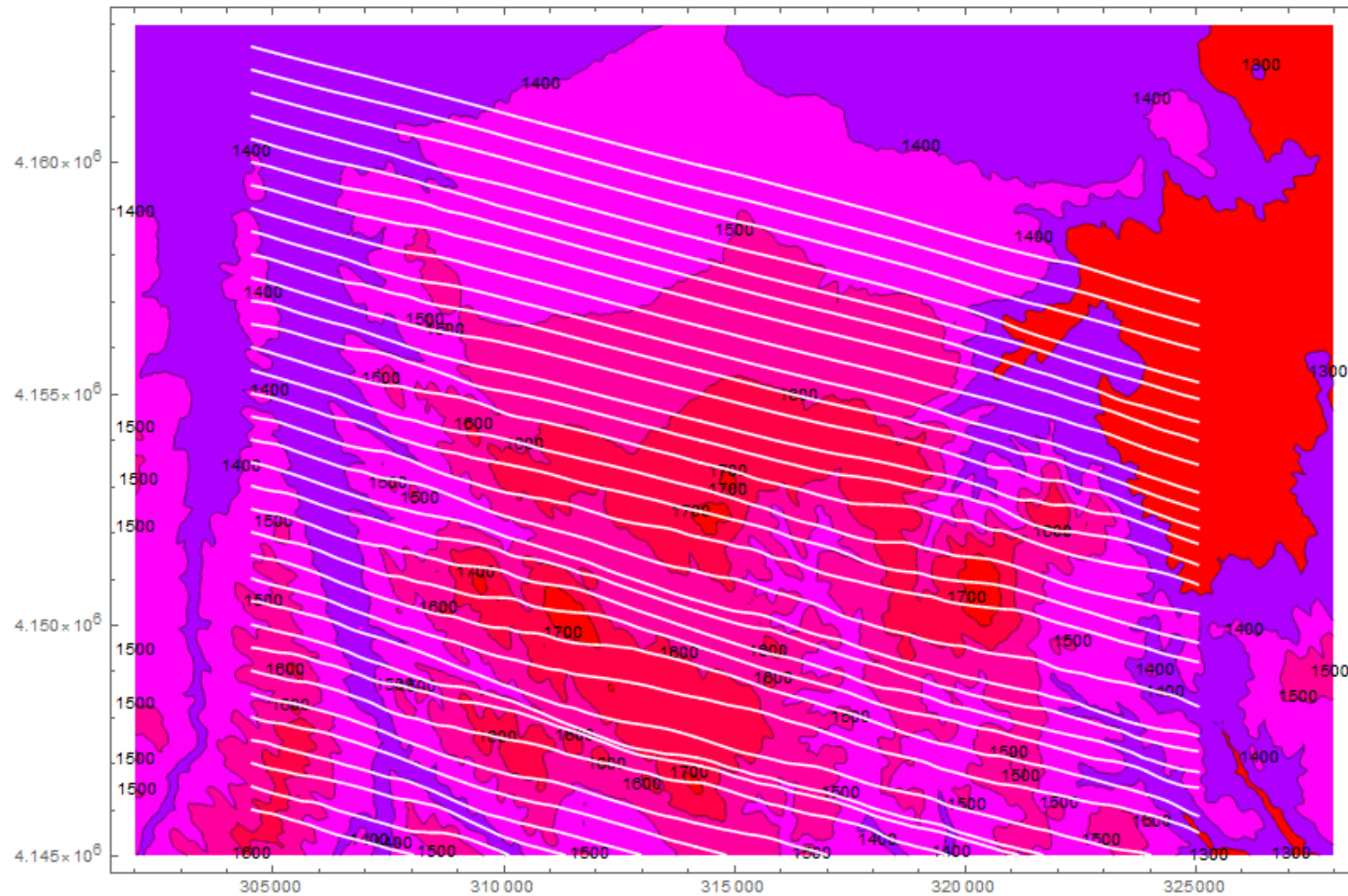
Fast computation of streamlines and speedup (1)

- Fuga “classic”:
 - Linearised CFD RANS code formulated in mixed spectral domain
 - Appr. 1.000.000 times faster than conventional (non-linear) CFD RANS
 - No numerical diffusion
- Fuga adapted to “moderately” complex terrain:
 - Only the linearized equations (**first order perturbation** in Cartesian terrain **height h**) have been considered
 - The trick is to transform to a **phony, flat world** - using a phony farm layout ... and perform computations here
 - The phony streamlines are completely **straight**, but they will follow the hills when transformed back to the physical world

Fast computation of streamlines and speedup (2)



Fast computation of streamlines and speedup (3)



Conclusions

- Framework for medium-fidelity **wake dynamics** in “moderately” complex terrain formulated ... as based on five simplifying conjectures
- Fast computation of **streamlines** and **speedup** facilitated using a linearized RANS model ... adapted to “moderately” complex terrain using first order perturbation theory

Future work

- Quantify the extension of the speed-up regime!
- The present streamline analysis is planned to be extended from a 2D Gaussian hill to a 3D Gaussian hill ... and for more wind speeds
- Present offshore-like WT replaced by a higher WT
- Turbulence in complex terrain may be spatially inhomogeneous ... which should be investigated
- ABL stability may have a role in definition of “moderately” complex terrain/re-circulation ... this should be checked

Acknowledgements

The EUDP project “Optimized layouts for wind farms in complex terrain - FARMOPT”, under contract 64013-0405, is acknowledged for financial support and thus for making this study possible